

Research Article

Decomposition of Fourth-Order Euler-Type Linear Time-Varying Differential System into Cascaded Two Second-Order Euler Commutative Pairs

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This paper presents decomposition of the fourth-order Euler-type linear time-varying system (LTVS) as a commutative pair of two second-order Euler-type systems. All necessary and sufficient conditions for the decomposition are deployed to investigate the commutativity, sensitivity, and the effect of disturbance on the fourth-order LTVS. Some systems are commutative, and some are not commutative, while some are commutative under certain conditions. Based on this fact, the commutativity of fourth-order Euler-type LTVS is investigated by introducing the commutative requirements, theories, and conditions. The fourth-order Euler-type LTVSs are investigated into commutative pairs of twice Euler-type second-order linear time-varying systems (LTVSs). The decomposition theories and conditions are derived, proved, and solved to simplify the use of commutativity for practical and industrial uses. Some fourth-order systems are sensitive toward change in initial conditions or parameters while others are not, and the effect due to disturbance also varies within systems. Furthermore, the stability and robustness of systems have so many issues. But we consider fourth-order Euler-type LTVS to observe, investigate, and tackle these issues. Lastly, the realization of fourth-order LTVS from cascaded two second-order systems can be laboratory experimented which is an open problem for future engineers to investigate. However, the theoretical results show a good agreement with the simulation results is considered in this work. Perhaps it might have unlimited physical applications in science and engineering as well as theoretical contribution. But beyond any reasonable doubt, the novelty is guaranteed because this study is the first of its kind that introduces the decomposition of the fourth-order Euler-type linear time-varying system (LTVS) as a commutative pair of two second-order Euler-type systems. Illustrative examples are presented to support the results.

1. Introduction

The important feature of cascade-connected systems motivates scientists and engineers to use the stability analysis of the connected system for the modelling of many physical problems and designing engineering systems. The order of connection plays a vital role in realizing more stable systems in electronics and electrical engineering. Hence, the commutativity concept has a significant role in the engineering point of view. In 1977, Marshall in [1] investigated the commutativity for 1st order continuous LTVSs. Later on, Koksál investigated the 2nd order [2] and 3rd order [3]

continuous LTVSs. Recently, Ibrahim and Koksál in [4] investigated the commutativity and sensitivity of Euler and Onsager 6th order LTVSs.

Decomposition is an essential mechanism that is used in many differential systems for developing the stability of a system and resolving physical problems. It is the process of splitting a high-order linear system into lower-order commutative pairs.

Decomposition formulas for 2nd order continuous-time LTVS were proved in [5] in 2016 by Koksál. The theoretical results and application for the realization of the 4th order LTVS were studied in [6] by Ibrahim and Koksál.

Transitivity property of commutativity for second-order linear time-varying analogue systems was studied in [7].

When it comes to fractional-order dynamic system and experimental aspects using analogue electronic devices that are reprogrammable, the decomposition of Laplace expressions into cascaded connections of small blocks makes possible a more reliable circuit design as shown in [8]. In this work, it can be noted that the orders of the blocks matter because the filter response may mitigate some frequencies that may be required by the next block.

In this paper, the commutativity, decomposition, sensitivity, and the effect of disturbance on the fourth-order Euler-type LTVSs are considered. Furthermore, the cases of nonzero initial conditions (ICs) are considered.

This paper is organized as follows. The mathematical materials and methods that introduce the commutativity conditions are considered in Section 2. The commutative requirements and conditions along with their general solution are provided in Section 3. Results and discussions for 4th order Euler LTVS are observed in Section 4. Section 5 demonstrates and illustrates the effectiveness of the results by considering fourth-order Euler-type LTVS. Finally, the results are concluded in Section 6.

2. Mathematical Materials and Methods

Let C be the fourth-order Euler LTVS, described by

$$C: C_4(t)t^4 y^{(4)}(t) + C_3(t)t^3 y^{(3)}(t) + C_2(t)t^2 y''(t) + C_1(t)t y'(t) + C_0(t)y(t) = x(t), \quad (1)$$

where the input and output are $x(t)$ and $y(t)$ and $C_i(t)$ represent the coefficients of the time-varying system, which are piecewise continuous functions on $[t_0, \infty)$. Let the initial conditions be $y(t_0)$, $y'(t_0)$, $y''(t_0)$, and $y^{(3)}(t_0)$ at the initial time $t_0 \in R$. Due to its order of 4, $C_4(t) \equiv 0$. The decomposition of C as the cascade connection of second-order systems A and B is given as

$$\begin{aligned} A: a_2(t)y_A''(t) + a_1(t)y_A'(t) + a_0(t)y_A(t) &= x_A(t), \\ B: b_2(t)y_B''(t) + b_1(t)y_B'(t) + b_0(t)y_B(t) &= x_B(t), \end{aligned} \quad (2)$$

with ICs

$$\begin{aligned} y_A(t_0), y_A'(t_0), \\ y_B(t_0), y_B'(t_0), \end{aligned} \quad (3)$$

where $a_2(t) \neq 0$ and $b_2(t) \neq 0$. Additionally, a_i , b_i , x_A , $x_B \in P[t_0, \infty)$.

The systems A and B are called commutative, while (A, B) represents the commutative pair provided that the input-output relations of AB and BA are equivalent.

For the cascade connection AB in Figure 1(a), the authors in [6] obtained a 4th order LTVS for the connection AB as

$$a_2 b_2 y^{(4)} + (a_2 b_1 + a_1 b_2 + 2a_2 b_2') y^{(3)} + (a_1 b_1 + a_0 b_2 + a_2 b_0 + 2a_2 b_1' + a_1 b_2' + a_2 b_2'') y'' \quad (4)$$

$$+ (a_0 b_1 + a_1 b_0 + 2a_2 b_0' + a_1 b_1' + a_2 b_1'') y' + (a_0 b_0 + a_1 b_0' + a_2 b_0'') y = x,$$

$$y(t_0) = y_B(t_0), \quad (5)$$

$$y'(t_0) = y_B'(t_0), \quad (6)$$

$$y''(t_0) = y_B''(t_0) = \frac{y_A(t_0) - b_0(t_0)y_B(t_0) - b_1(t_0)y_B'(t_0)}{b_2(t_0)}, \quad (7)$$

$$\begin{aligned} y^{(3)}(t_0) = y_B^{(3)}(t_0) = & \left(-\frac{b_1(t_0)}{b_2^2(t_0)} - \frac{b_2'(t_0)}{b_2^2(t_0)} \right) y_A(t_0) + \frac{1}{b_2(t_0)} y_A'(t_0) \\ & + \left(\frac{b_0(t_0)b_1(t_0)}{b_2^2(t_0)} + \frac{b_0(t_0)b_2'(t_0)}{b_2^2(t_0)} - \frac{b_0'(t_0)}{b_2(t_0)} \right) y_B(t_0) \\ & + \left(\frac{b_1^2(t_0)}{b_2^2(t_0)} + \frac{b_1(t_0)b_2'(t_0)}{b_2^2(t_0)} - \frac{b_0(t_0)}{b_2(t_0)} - \frac{b_1'(t_0)}{b_2(t_0)} \right) y_B'(t_0). \end{aligned} \quad (8)$$

Interchanging $A \leftrightarrow B$ and $a \leftrightarrow b$ from Figure 1(b), the connection BA provides the following results:

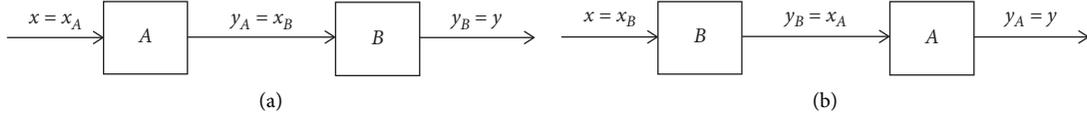


FIGURE 1: Cascade connection of the LTVSs.

$$b_2 a_2 y^{(4)} + (b_2 a_1 + b_1 a_2 + 2b_2 a_2') y^{(3)} + (b_1 a_1 + b_0 a_2 + b_2 a_0 + 2b_2 a_1' + b_1 a_2' + b_2 a_2'') y'' + (b_0 a_1 + b_1 a_0 + 2b_2 a_0' + b_1 a_1' b_2 a_1'') y' + (a_0 b_0 + b_1 a_0' + b_2 a_0'') y = x, \quad (9)$$

$$y(t_0) = y_A(t_0), \quad (10)$$

$$y'(t_0) = y_A'(t_0), \quad (11)$$

$$y''(t_0) = y_A''(t_0) = \frac{y_B(t_0) - a_0(t_0)y_A(t_0) - a_1(t_0)y_A'(t_0)}{a_2(t_0)}, \quad (12)$$

$$y^{(3)}(t_0) = y_A^{(3)}(t_0) = \left[\frac{a_1(t_0)}{a_2^2(t_0)} - \frac{a_2'(t_0)}{a_2^2(t_0)} \right] y_B(t_0) + \frac{1}{a_2(t_0)} y_B'(t_0) + \left[\frac{a_1^2(t_0)}{a_2^2(t_0)} + \frac{a_1(t_0)a_2'(t_0)}{a_2^2(t_0)} - \frac{a_0(t_0)}{a_2(t_0)} - \frac{a_1'(t_0)}{a_2(t_0)} \right] y_A'(t_0) + \left[\frac{a_0(t_0)a_1(t_0)}{a_2^2(t_0)} + \frac{a_0(t_0)a_2'(t_0)}{a_2^2(t_0)} - \frac{a_0'(t_0)}{a_2(t_0)} \right] y_A(t_0). \quad (13)$$

3. Commutativity Requirements

Two 2nd order LTVS subsystems A and B are called commutative if the connections AB and BA are identical. Regarding this case, the equivalence is realized iff differential equations in equations (4) and (9) are the same; in addition to the initial conditions in equations (5)–(8) and equations (10)–(13) must be the same. Solving equations (4) and (9) for b_2, b_1, b_0 yields the matrix system

$$\begin{bmatrix} b_2 \\ b_1 \\ b_0 \end{bmatrix} = \begin{bmatrix} a_2 & 0 & 0 \\ a_1 & a_2^{0.5} & 0 \\ a_0 & f_{32} & 1 \end{bmatrix} \begin{bmatrix} k_2 \\ k_1 \\ k_0 \end{bmatrix}, \quad (14)$$

$$f_{32} = \frac{1}{4} [a_2^{-0.5} (2a_1 - a_2')],$$

where k_2, k_1, k_0 are some constants. Furthermore, coefficients of the differential form of A satisfy

$$-a_2^{0.5} \frac{d}{dt} \left[a_0 - \frac{4a_1^2 + 3a_2'^2 - 8a_1 a_2' + 8a_1' a_2 - 4a_2' a_2''}{16a_2} \right] k_1 = 0, \quad \forall t \geq t_0. \quad (15)$$

Commutativity with arbitrary and nonzero initial conditions can be assured by considering equations (16)–(22) (for more details, see [6]):

$$y = y_B = y_A, \quad (16)$$

$$y' = y_B' = y_A', \quad (17)$$

$$y'' = \left(\frac{1}{b_2} - \frac{b_0}{b_2} \right) y_A - \frac{b_1 y_A'}{b_2} = \left(\frac{1}{a_2} - \frac{a_0}{a_2} \right) y_A - \frac{a_1 y_A'}{a_2}, \quad (18)$$

$$\begin{aligned}
y^{(3)} &= \left(-\frac{b_1}{b_2^2} - \frac{b_2'}{b_2^2} \right) y_A + \left(\frac{b_0 b_1}{b_2^2} - \frac{b_0'}{b_2} + \frac{b_0 b_2'}{b_2^2} \right) y_B + \frac{1}{b_2} y_A' + \left(\frac{b_1^2}{b_2^2} - \frac{b_0}{b_2} - \frac{b_1'}{b_2} + \frac{b_1 b_2'}{b_2^2} \right), \\
&= \left(\frac{a_0 a_1}{a_2^2} - \frac{a_0'}{a_2} + \frac{a_0 a_2'}{a_2^2} \right) y_A + \left(\frac{a_1^2}{a_2^2} - \frac{a_0}{a_2} - \frac{a_1'}{a_2} + \frac{a_1 a_2'}{a_2^2} \right) y_A' + \left(-\frac{a_1}{a_2^2} - \frac{a_2'}{a_2^2} \right) y_B + \frac{1}{a_2} y_B',
\end{aligned} \tag{19}$$

$$\left(-\frac{1}{a_2} + \frac{1}{a_2 k_2} - \frac{k_0}{a_2 k_2} - \frac{a_1 k_1}{2a_2^{3/2} k_2} + \frac{k_1 a_2'}{4a_2^{3/2} k_2} \right) y_A - \frac{k_1 y_A'}{\sqrt{a_2} k_2} = 0, \tag{20}$$

$$\begin{aligned}
&\left[\begin{array}{l} \frac{a_1}{a_2^2} - \frac{k_1}{a_2^{3/2} k_2} - \frac{a_1}{a_2^2 k_2} + \frac{k_0 k_1}{a_2^{3/2} k_2^2} + \frac{a_1 k_1^2}{2a_2^2 k_2^2} + \frac{a_1 k_0}{a_2^2 k_2} + \frac{a_1^2 k_1}{2a_2^{5/2} k_2} + \frac{a_0 k_1}{a_2^{3/2} k_2} \\ \frac{k_1 a_1'}{2a_2^{3/2} k_2} + \frac{a_2'}{a_2^2} - \frac{a_2'}{a_2^2 k_2} + \frac{a_1 k_1 a_2'}{2a_2^2 k_2} - \frac{k_1^2 a_2'}{4a_2^2 k_2^2} + \frac{k_0 a_2'}{a_2^2 k_2} - \frac{3k_1 (a_2')^2}{8a_2^{5/2} k_2} + \frac{k_1 a_1''}{4a_2^{3/2} k_2} \end{array} \right] y_A \\
&+ \left(-\frac{1}{a_2} + \frac{k_1^2}{a_2 k_2^2} + \frac{1}{a_2 k_2} + \frac{3a_1 k_1}{2a_2^{3/2} k_2} - \frac{k_0}{a_2 k_2} + \frac{3k_1 a_2'}{4a_2^{3/2} k_2} \right) y_A' = 0,
\end{aligned} \tag{21}$$

$$(k_0 + k_2 - 1) = 0. \tag{22}$$

4. Results and Discussion

In this section, the explicit commutative formulas obtained from the previous section are considered, and the coefficients of the decompositions A and B are expressed in terms of the decomposed fourth-order Euler system C . Observe that (1) and (4) are both 4th order LTVSs, and the equivalent relation between them leads to

$$a_2 b_2 = C_4 t^4 = a_2^2 k_2 = C_4 t^4 \longrightarrow a_2 = t^2 \left(\frac{C_4}{k_2} \right)^{1/2}. \tag{23}$$

Comparing the coefficients of the 3rd derivatives and making use of (14) leads to

$$a_1 = \frac{1}{2} \left[-\frac{C_4'}{\sqrt{C_4} \sqrt{k_2}} t^2 + \left(-\frac{C_4^{1/4} k_1}{k_2^{5/4}} + \frac{C_3}{\sqrt{C_4} \sqrt{k_2}} - \frac{4\sqrt{C_4}}{\sqrt{k_2}} \right) t \right]. \tag{24}$$

Relating the coefficients of the 2nd derivatives and making use of (14) gives

$$a_0 = \frac{1}{16} \left[\begin{array}{l} \left(\frac{2(C_4')^2}{C_4^{3/2} k_2^{3/4}} - \frac{4(C_4')^2}{C_4^{3/2} \sqrt{k_2}} - \frac{4C_4''}{\sqrt{C_4} k_2^{3/4}} + \frac{8C_4''}{\sqrt{C_4} \sqrt{k_2}} \right) t^2 \\ + \left(-\frac{8C_3'}{\sqrt{C_4} \sqrt{k_2}} + \frac{3k_1 C_4'}{C_4^{3/4} k_2^{5/4}} - \frac{16C_4'}{\sqrt{C_4} k_2^{3/4}} + \frac{6C_3 C_4'}{C_4^{3/2} \sqrt{k_2}} + \frac{32C_4'}{\sqrt{C_4} \sqrt{k_2}} \right) t \\ + \frac{4k_1^2}{k_2^2} - \frac{2C_3 k_1}{C_4^{3/4} k_2^{5/4}} + \frac{12C_4^{1/4} k_1}{k_2^{5/4}} - \frac{16\sqrt{C_4}}{k_2^{3/4}} - \frac{2C_3^2}{C_4^{3/2} \sqrt{k_2}} + \frac{8C_2}{\sqrt{C_4} \sqrt{k_2}} + \frac{32\sqrt{C_4}}{\sqrt{k_2}} - \frac{8k_0}{k_2} \end{array} \right]. \tag{25}$$

Considering the obtained results a_2 , a_1 , and a_0 of equations (23)–(25), respectively, we figure out b_2 , b_1 , b_0 using (14) and present them in the following explicit forms:

$$b_2 = k_2^{1/2} c_4^{1/2} t^2, \quad (26)$$

$$b_1 = \frac{1}{2} \left[-\frac{\sqrt{k_2} C_4' t^2}{\sqrt{C_4}} + \left(\frac{C_4^{1/4} k_1}{k_2^{1/4}} + \frac{C_3 \sqrt{k_2}}{\sqrt{C_4}} - 4\sqrt{C_4} \sqrt{k_2} \right) t \right], \quad (27)$$

$$b_0 = \frac{1}{16} \left[\begin{aligned} & \left(\frac{2k_2^{1/4} (C_4')^2}{C_4^{3/2}} - \frac{4\sqrt{k_2} (C_4')^2}{C_4^{3/2}} - \frac{4k_2^{1/4} C_4''}{\sqrt{C_4}} + \frac{8\sqrt{k_2} C_4''}{\sqrt{C_4}} \right) t^2 \\ & + \left(-\frac{8\sqrt{k_2} C_3'}{\sqrt{C_4}} - \frac{3k_1 C_4'}{C_4^{3/4} k_2^{1/4}} - \frac{16k_2^{1/4} C_4'}{\sqrt{C_4}} + \frac{6C_3 \sqrt{k_2} C_4'}{C_4^{3/2}} + \frac{32\sqrt{k_2} C_4'}{\sqrt{C_4}} \right) t + 8k_0 \\ & + \frac{2C_3 k_1}{C_4^{3/4} k_2^{1/4}} - \frac{12C_4^{1/4} k_1}{k_2^{1/4}} - 16\sqrt{C_4} k_2^{1/4} - \frac{2C_3^2 \sqrt{k_2}}{C_4^{3/2}} + \frac{8C_2 \sqrt{k_2}}{\sqrt{C_4}} + 32\sqrt{C_4} \sqrt{k_2} \end{aligned} \right]. \quad (28)$$

From (1) and (4), one needs to observe the following equations:

$$tC_1 = a_0 b_1 + a_1 b_0 + 2a_2 b_0' + a_1 b_1' + a_2 b_1'', \quad (29)$$

$$C_0 = (a_0 b_0 + a_1 b_0' + a_2 b_0''). \quad (30)$$

Substituting the coefficients $a_2, a_1, a_0, b_2, b_1,$ and b_0 from (23)–(28) into (29) and (30), after numerous mathematical computations and comparative analysis, the following requirements are acquired:

$$C_1 = \frac{1}{8} \left(-16C_2 - \frac{C_3^3}{C_4^2} + \frac{4C_2 C_3}{C_4} + \frac{6C_3^2}{C_4} - 32C_4 + \frac{C_4^{1/4} k_1^3}{k_2^{9/4}} - \frac{8C_3}{k_2^{1/4}} + \frac{32C_4}{k_2^{1/4}} - \frac{4C_4^{1/4} k_0 k_1}{k_2^{5/4}} \right), \quad (31)$$

$$C_0 = \frac{1}{256} \left(\begin{aligned} & 5512C_2 + \frac{4C_3^4}{C_4^3} - \frac{32C_2 C_3^2}{C_4^2} + \frac{64C_2^2}{C_4} - \frac{128C_3^2}{C_4} + 1024C_4 + \frac{8C_3 k_1^3}{C_4^{3/2} k_2^{9/4}} - \frac{48C_4^{1/4} k_1^3}{k_2^{9/4}} \\ & + \frac{32k_0 k_1^2}{k_2^2} - \frac{64\sqrt{C_4} k_1^2}{k_2^{7/4}} - \frac{12C_3^2 k_1^2}{C_4^{3/2} k_2^{3/2}} + \frac{32C_2 k_1^2}{\sqrt{C_4} k_2^{3/2}} + \frac{48C_3 k_1^2}{\sqrt{C_4} k_2^{3/2}} - \frac{16\sqrt{C_4} k_1^2}{k_2^{3/2}} - \frac{32C_3 k_0 k_1}{C_4^{3/4} k_2^{5/4}} \\ & + \frac{192C_4^{1/4} k_0 k_1}{k_2^{5/4}} - \frac{64k_0^2}{k_2} + \frac{256C_4}{\sqrt{k_2}} - \frac{256C_2}{k_2^{1/4}} + \frac{64C_3^2}{C_4 k_2^{1/4}} - \frac{1024C_4}{k_2^{1/4}} \end{aligned} \right). \quad (32)$$

Theorem 1. *The necessary and sufficient conditions for Euler 4th-order LTVS of equation (1) to be decomposed into cascade-connected LTV commutative pairs of Euler 2nd-order are that*

- (i) *There exist some constants k_2, k_1, k_0 such that the coefficients C_1 and C_0 can be formulated in connection with $C_4, C_3,$ and C_2 as in (31) and (32), respectively,*
- (ii) *The reduced Euler 2nd order A and B must be formulated with regard to $C_4, C_3,$ and C_2 as in equations (23)–(28).*

Proof. The detailed proof of (i) of Theorem 1 can be seen in equations (29) and (30), while in (ii) of Theorem 1, equations

(23)–(28) are obtained from the coefficients of equations (1) and (4).

Note. Theorem 1 is applicable to the zero IC case. Regarding the case of nonzero ICs, it is covered in Theorem 2. \square

Theorem 2. *The necessary and sufficient conditions for the decomposition of Euler 4th order LTVS C with nonzero ICs into its twin Euler 2nd order LTV commutative pairs A and B are that*

- (i) *The requirements of Theorem 1 are fulfilled.*
- (ii) *The ICs of A, B, C must obey equations (16) and (17).*
- (iii) *Furthermore, the ICs of A must obey equations (20) and (21).*
- (iv) *In addition, the ICs of C must be satisfied.*

$$y''(t_0) = \left[\begin{array}{l} \frac{2}{t^2} + \frac{C_3^2}{8t^2 C_4^2} - \frac{C_2}{2t^2 C_4} - \frac{k_1^2}{4t^2 \sqrt{C_4} k_2^{3/2}} + \frac{C_3 k_1}{8t^2 C_4^{5/4} k_2^{3/4}} - \frac{3k_1}{4t^2 C_4^{1/4} k_2^{3/4}} + \frac{k_0}{2t^2 \sqrt{C_4} \sqrt{k_2}} + \\ \frac{1}{t^2 k_2^{1/4}} + \frac{\sqrt{k_2}}{t^2 \sqrt{C_4}} + \frac{C_3'}{2t C_4} - \frac{3C_3 C_4'}{8t C_4^2} - \frac{2C_4'}{t C_4} - \frac{3k_1 C_4'}{16t C_4^{5/4} k_2^{3/4}} + \frac{C_4'}{t C_4 k_2^{1/4}} + \frac{(C_4')^2}{4C_4^2} - \frac{(C_4')^2}{8C_4^2 k_2^{1/4}} - \frac{C_4''}{2C_4} + \frac{C_4''}{4C_4 k_2^{1/4}} \end{array} \right] y_A(t_0), \quad (33)$$

$$y^{(3)}(t_0) = \left[\begin{array}{l} -\frac{C_3^3}{16t^3 C_4^3} + \frac{C_2 C_3}{4t^3 C_4^2} + \frac{C_3}{t^3 C_4} - \frac{k_1^3}{8t^3 C_4^{3/4} k_2^{9/4}} + \frac{3C_3 k_1^2}{16t^3 C_4^{3/2} k_2^{3/2}} - \frac{3k_1^2}{8t^3 \sqrt{C_4} k_2^{3/2}} + \frac{k_0 k_1}{4t^3 C_4^{3/4} k_2^{5/4}} \\ + \frac{k_1}{2t^3 C_4^{1/4} k_2} - \frac{C_2 k_1}{4t^3 C_4^{5/4} k_2^{3/4}} + \frac{3C_3 k_1}{8t^3 C_4^{5/4} k_2^{3/4}} - \frac{k_1}{t^3 C_4^{1/4} k_2^{3/4}} - \frac{C_3 k_0}{4t^3 C_4^{3/2} \sqrt{k_2}} - \frac{C_3}{2t^3 C_4 k_2^{1/4}} \\ + \frac{k_1}{2t^3 C_4^{3/4} k_2^{1/4}} - \frac{C_3 \sqrt{k_2}}{2t^3 C_4^{3/2}} - \frac{C_2'}{2t^2 C_4} - \frac{C_3 C_3'}{4t^2 C_4^2} + \frac{C_3'}{2t^2 C_4} + \frac{3k_1 C_3'}{8t^2 C_4^{5/4} k_2^{3/4}} + \frac{C_3 \sqrt{k_2} C_3'}{4t^2 C_4^2} \\ + \frac{3C_3^2 C_4'}{16t^2 C_4^3} + \frac{C_2 C_4'}{4t^2 C_4^2} + \frac{5C_3 C_4'}{8t^2 C_4^2} - \frac{3C_4'}{t^2 C_4} - \frac{3k_1^2 C_4'}{32t^2 C_4^{3/2} k_2^{3/2}} + \frac{k_1 C_4'}{2t^2 C_4^{5/4} k_2} - \frac{3C_3 k_1 C_4'}{16t^2 C_4^{9/4} k_2^{3/4}} + \frac{3C_4'}{2t^2 C_4 k_2^{1/4}} - \frac{11k_1 C_4'}{8t^2 C_4^{5/4} k_2^{3/4}} \\ - \frac{C_3 C_4'}{2t^2 C_4^2 k_2^{1/4}} - \frac{3C_3^2 \sqrt{k_2} C_4'}{16t^2 C_4^3} - \frac{5C_3' C_4'}{8t C_4^2} + \frac{7C_3 (C_4')^2}{16t C_4^3} + \frac{3(C_4')^2}{2t C_4^2} - \frac{k_1 (C_4')^2}{16t C_4^{9/4} k_2} + \frac{17k_1 (C_4')^2}{64t C_4^{9/4} k_2^{3/4}} + \frac{C_3 (C_4')^2}{16t C_4^3 k_2^{1/4}} - \frac{(C_4')^2}{4t C_4^2 k_2^{1/4}} - \frac{3(C_4')^3}{8C_4^3} \\ + \frac{3(C_4')^3}{16C_4^3 k_2^{1/4}} + \frac{C_4''}{2t C_4} - \frac{C_3 C_4''}{8t C_4^2} - \frac{3C_4''}{t C_4} + \frac{k_1 C_4''}{8t C_4^{5/4} k_2} - \frac{7k_1 C_4''}{16t C_4^{5/4} k_2^{3/4}} - \frac{C_3 C_4''}{8t C_4^2 k_2^{1/4}} + \frac{3C_4''}{2t C_4 k_2^{1/4}} + \frac{3C_4' C_4''}{4C_4^2} - \frac{3C_4' C_4''}{8C_4^2 k_2^{1/4}} - \frac{C_4^{(3)}}{2C_4} + \frac{C_4^{(3)}}{4C_4 k_2^{1/4}} \end{array} \right] y_A(t_0) \\ + \left[\begin{array}{l} \left[\frac{3C_3^2}{8t^2 C_4^2} - \frac{C_2}{2t^2 C_4} - \frac{3C_3}{2t^2 C_4} - \frac{3C_3 k_1}{8t^2 C_4^{5/4} k_2^{3/4}} + \frac{1}{t^2 k_2^{1/4}} + \frac{3k_1}{4t^2 C_4^{1/4} k_2^{3/4}} + \frac{k_0}{2t^2 \sqrt{C_4} \sqrt{k_2}} \right] y_A'(t_0). \\ + \frac{\sqrt{k_2}}{t^2 \sqrt{C_4}} - \frac{3C_3 C_4'}{8t C_4^2} + \frac{3k_1 C_4'}{16t C_4^{5/4} k_2^{3/4}} + \frac{C_4'}{t C_4 k_2^{1/4}} - \frac{(C_4')^2}{8C_4^2 k_2^{1/4}} + \frac{C_4''}{4C_4 k_2^{1/4}} \end{array} \right] \quad (34)$$

(v) For $k_1 = 0$, the ICs must satisfy (22).

Proof. Theorem 2 (i) is obvious; for Theorem 2 (ii), the ICs in equations (16) and (17) are obtained from equations (5), (10) and equation (6), (11), respectively. Patterning Theorem 2(iii), the ICs in equations (20) and (21) are obtained from equations (7), (12) and equations (8), (13), respectively.

Regarding equation (33), we consider equation (18); inserting in values of a_2 , a_1 , and a_0 of equations (23)–(25) leads to equation (33). Equation (34) is obtained by using equation (19); substituting the values of a_2 , a_1 , and a_0 of equations (23)–(25), respectively, in equation (19) provides equation (34). Item (v) results from equation (22) as the solution of equations (20) and (21). \square

5. Applications to Fourth-Order Euler-Type LTVS

We apply the results obtained from the previous sections to investigate the decomposition of fourth-order Euler LTVS as a commutative pair of two second-order Euler-type systems.

5.1. Example 1. Considering the constants $C_4 = C_3 = C_2 = 1$, with k_i 's in equation (36), $C_1 = -15/8$ and $C_0 = 299/192$ are obtained by making use of equations (31) and (32), respectively. The general Euler-type fourth-order LTVS C of equation (1) becomes

$$t^4 y^{(4)}(t) + t^3 y^{(3)}(t) + t^2 y''(t) - \frac{15}{8} t y'(t) + \frac{299}{192} y(t) = x(t). \quad (35)$$

Note that equation (22) is satisfied with the constants

$$k_2 = 3, k_1 = 0, k_0 = -2. \quad (36)$$

Furthermore, equations (16)–(19) lead to

$$y_B(t_0) = y_A(t_0) = y(t_0), \quad (37)$$

$$y_B'(t_0) = y_A'(t_0) = y'(t_0), \quad (38)$$

$$y''(t_0) = \left(-\frac{11}{8} + \frac{2}{\sqrt{3}} \right) y(t_0) + \frac{3}{2} y'(t_0) \text{ for } t_0 = 1, \quad (39)$$

$$y^{(3)}(t_0) = \left(\frac{11}{16} - \frac{1}{\sqrt{3}}\right)y(t_0) + \left(-\frac{5}{8} + \frac{2}{\sqrt{3}}\right)y'(t_0) \text{ for } t_0 = 1. \quad (40)$$

The Euler subsystems A and B generate the equations

$$A: \frac{t^2}{\sqrt{3}}y_A''(t) - \frac{\sqrt{3}}{2}ty_A'(t) + \left(\frac{33 + 8\sqrt{3}}{24\sqrt{3}}\right)y_A(t) = x_A(t), \quad (41)$$

$$B: \sqrt{3}t^2y_B'(t) - \frac{3\sqrt{3}}{2}ty_B'(t) + \left(\frac{11\sqrt{3} - 8}{8}\right)y_B(t) = x_B(t). \quad (42)$$

Note that both subsystems A and B in the decomposition are of Euler type. Simulation was carried out with a sinusoid of frequency 3 rad/sec, amplitude 2, and bias $-21/10$, considering ode (Bogacki–Shampine) as the solver, while maintaining a fixed step length of 0.01. Simulink outcomes

are illustrated in Figure 2. The initial time and initial states chosen are $t_0 = 1$ and $y(1) = y_A(1) = y_B(1) = y'_B(1) = y'_A(1) = y'(1) = 0.5$. Equations (39) and (40) lead to $y''(1) = 1/16 + 1/\sqrt{3}$, $y^{(3)}(1) = 1/32 + 1/2\sqrt{3}$. After satisfying all decomposition conditions, the systems AB , BA , and C produce a similar response ($B = BA = C$, see Figure 2). However, with a small modification in the decomposition requirement by changing $y_B(1) = y_A(1) = y(1) = 0.5$ to $y_A(1) = y(1) = 0.6$, then equation (37) is not satisfied, and the decomposition is messed up, and it is not valid any more (see $AB1$, $BA1$, $C1$ in Figure 2). Observe that $AB1$ is slightly disturbed by the changes, while $BA1$ is so sensitive to ICs. Therefore, A and B should be connected in the cascade synthesis of C .

5.2. *Example 2.* In this example, the 4th order LTVS C is reconstructed by considering the 2nd order subsystem A . In line with this, consider the 2nd order LTVS A defined by

$$A: y_A''(t) + \sin(t)y_A'(t) + \left(\frac{\sin^2(t)}{4} + \frac{\sin(t)}{\sqrt{5}} + \frac{\cos(t)}{2} + \frac{3}{4}\right)y_A(t) = x_A(t). \quad (43)$$

For the constant k_1 :

$$\frac{1}{k_2^2} \begin{bmatrix} k_2 - k_2k_0 - k_2^2 - 0.5k_2k_1t & -k_1k_2 \\ k_0k_1 - k_1 - 0.5k_2k_1 + V & k_1^2 + k_2 - k_2k_0 - k_2^2 + 1.5k_2k_1t \end{bmatrix} \begin{bmatrix} y_A \\ y_A' \end{bmatrix} = 0, \quad (44)$$

where $V = (1 - k_2 + 0.5k_1^2 + k_2k_0)t + 0.25k_2k_1t^2$.

For the commutativity with nonzero ICs, the coefficient matrix in equation (44) must be singular at $t_0 = 0$, that is, its determinant is zero if

$$k_1 = \mp \frac{2}{\sqrt{5}}(k_0 + k_2 - 1). \quad (45)$$

Furthermore, equation (44) at $t_0 = 0$ requires

$$(k_2 - k_2k_0 - k_2^2)y_A - k_1k_2y_A' = 0. \quad (46)$$

Inserting equation (45) into equation (46) guarantees commutativity of A and B :

$$y_A' = \pm \frac{\sqrt{5}}{2}y_A, \text{ with } y_A \text{ arbitrary.} \quad (47)$$

Consider the case $k_1 \neq 0$ and choose

$$k_2 = 1, k_1 = \mp \frac{2}{\sqrt{5}}, k_0 = 1. \quad (48)$$

By making use of equation (14), the pair B is obtained in terms of A :

$$B: y_B''(t) + \left(\sin(t) + \frac{2}{\sqrt{5}}\right)y_B'(t) + \left(\frac{\sin^2(t)}{4} + \frac{\sin(t)}{\sqrt{5}} + \frac{\cos(t)}{2} + \frac{3}{4}\right)y_B(t) = x_B(t). \quad (49)$$

Considering the coefficients b_2, b_1, b_0 of equation (49) and the system A , that is, a_2, a_1, a_0 from equation (43), we realize fourth-order LTVS C as

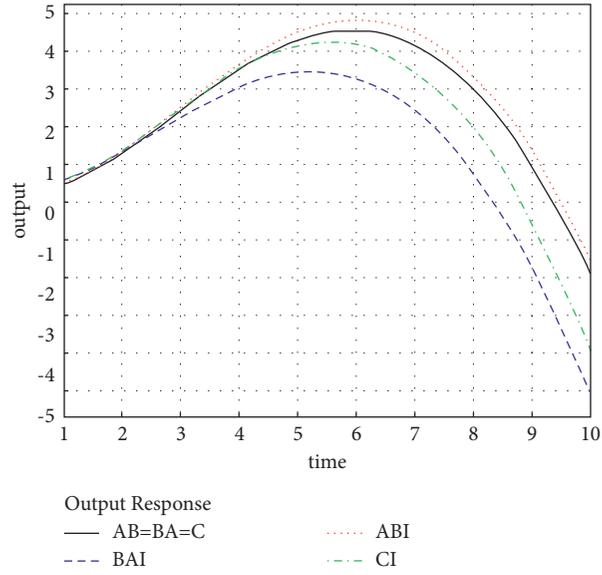


FIGURE 2: Simulation results of example 1.

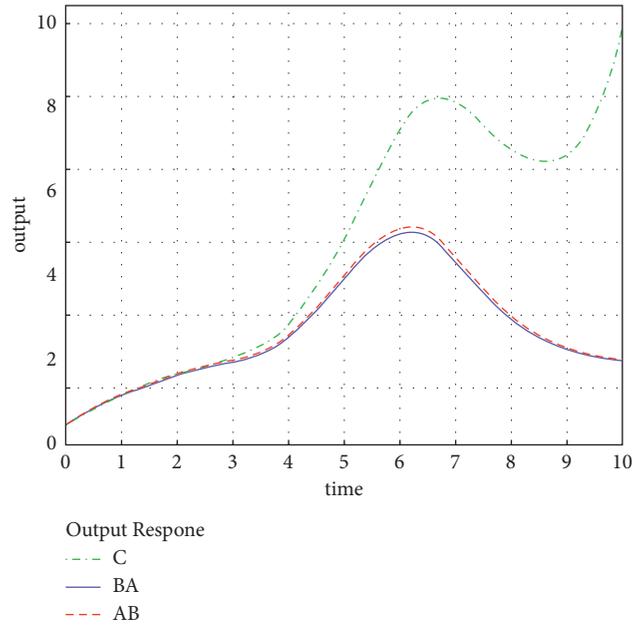


FIGURE 3: Simulation results of example 2.

$$\begin{aligned}
C: & y^{(4)}(t) + \left(2 \sin(t) + \frac{2}{\sqrt{5}}\right) y^{(3)}(t) \\
& + \left(\frac{3 \sin^2(t)}{2} + \frac{3 \sin(t)}{\sqrt{5}} + 3 \cos(t) + \frac{1}{2}\right) y''(t) \\
& + \left(\frac{\sin^3(t)}{2} + \frac{3 \sin^2(t)}{2\sqrt{5}} + 3 \cos(t) \sin(t) + \frac{3 \cos(t)}{\sqrt{5}} - \frac{3 \sin(t)}{2} - \frac{1}{2\sqrt{5}}\right) y'(t) \\
& + \left(\frac{\sin^4(t)}{16} + \frac{\sin^3(t)}{4\sqrt{5}} + \frac{3}{4} \cos(t) \sin^2(t) + \frac{3 \cos^2(t)}{4} - \frac{7 \sin^2(t)}{8} + \frac{3 \cos(t) \sin(t)}{2\sqrt{5}} - \frac{\cos(t)}{4} - \frac{\sqrt{5} \sin(t)}{4} - \frac{3}{16}\right)
\end{aligned} \tag{50}$$

$$y(t) = x(t).$$

Regarding the decomposition with nonzero initial condition, $y(t_0) \neq 0$, equations (16)–(19) yield

$$y_B(t_0) = y_A(t_0) = y(t_0), \quad (51)$$

$$y'_B(t_0) = y'_A(t_0) = y'(t_0) = \pm \frac{\sqrt{5}}{2} y_A(t_0), \quad (52)$$

$$y''_B(t_0) = y''(t_0) = \frac{3}{4} y(t_0) \text{ for } t_0 = 0, \quad (53)$$

$$y^{(3)}(t_0) = -\frac{1}{4} y'(t_0) \text{ for } t_0 = 0. \quad (54)$$

Simulations are carried out with a sinusoid of frequency 3 rad/sec, amplitude 3, and bias -0.5 . The rationale behind using Runge–Kutta as a solver was based on its numerical stability as well as accuracy. The Runge–Kutta schemes satisfy the possibility condition for any time-step interval “change in time” (see [9] and [10]). Simulink outcomes are illustrated in Figure 3. The initial time and initial conditions chosen are $t_0 = 0$ and $y(0) = y_A(0) = y_B(0) = -1$, respectively. Computing equations (52)–(54) leads to $y'_B(0) = y'_A(0) = y'(0) = \pm \sqrt{5}/2$, $y''(0) = -3/4$ and $y^{(3)} = -5/8\sqrt{5}$. The responses of system C and its decompositions as AB and BA give the same output as shown in Figure 3 (C). A noise signal in the form of saw-tooth wave (signal generator) with amplitude 0.05 and frequency 0.01 rad/sec is injected between the subsystems A and B . The simulation results are shown in Figure 3 (AB and BA).

6. Conclusion

The commutativity and decomposition of fourth-order Euler LTVS are considered as a commutative pair of two second-order Euler-type systems. The results are analyzed explicitly and depicted by simulations. Our results highlight the sensitivity of fourth-order Euler-type LTVSs as a result of changes in ICs and present the effect of disturbance due to external noise. Based on these findings, we investigated and discovered that the fourth-order Euler LTVS C possess its commutative pairs A and B which are obtained as a result of the decomposition process in Theorems 1 and 2 as well as in example 1. The commutative pairs A and B are commutative under certain conditions and can be used for the realization of fourth-order LTVS as seen in example 2. The fourth-order Euler LTVS C in equation (35) and the systems AB and BA of example 1 are sensible toward changes in ICs. Moreover, the system in equation (50) and the systems AB and BA of example 2 show great level of commutativity imbalance toward noise disturbance. Example 1 investigated the decomposition of fourth-order Euler-type LTVS, and our findings verify that fourth-order Euler-type LTVSs always have general decomposed commutative pairs which are also Euler-type systems. The Euler systems possess both constant forward feedback conjugates and non-constant feedback conjugates as commutative pairs. Also, they have less effect toward disturbance due to noise and are sensible toward change in ICs (see [4]). Example 2 presented second-order LTVS as a subsystem that is used for the realization of

fourth-order LTVS. The system has a great effect toward disturbance due to noise. These special properties of Euler systems make them a case of interest and differentiate them from other systems.

At last, one can easily observe that the theoretical results are in good agreement with the simulation results. Generalizing and applying these theorems in nonlinear systems, fractional systems, and partial differential systems is an open problem for future investigations. Hence, they remind system designers which connection order should be used in the cascade structure of system synthesis.

Data Availability

No data were used to support this study.

Conflicts of Interest

The authors declare that there are no conflicts of interest regarding the publication of this paper.

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